

# Ultra-linear power amplifier characterization using dynamic range extension techniques

## White Paper

### Abstract

The rapid growth of the wireless industry requires more efficient utilization of the available frequency spectrum. This has resulted in requirements for highly linear multi-channel power amplifiers (MCPAs) to support increases in voice and data traffic. To characterize the resulting ultra-linear MCPAs and to comply with inter-modulation levels less than  $-80$  dBc requires measurement systems with dynamic range performance beyond what is currently available. A new instrument, which extends the dynamic range of current distortion measurement systems by at least 25 dB, has been developed to meet this challenge.

### I. Introduction

Significant modulation format changes are on the way for wireless systems evolving to 3G. The goal of these format changes is to enable efficient data access over the wireless networks and to increase utilization of wireless communication for data as well as voice. Efficient data access requires enhanced air interface data rates and the European Telecommunications Standards Institute (ETSI) has set new standards for GSM, EDGE, and W-CDMA. EDGE (Enhanced Data rates for Global Evolution) moves GSM from GMSK to 8-PSK modulation, which increases the Peak to Average power Ratio (PAR) and significantly increases the linearity requirements of current GSM amplifier systems -- especially where multiple carriers are employed.

Table 1 summarizes the in-band spectral requirements for transmission of these signals in accordance with European Spectral requirements. For offsets  $>$  than 6 MHz from the carrier, spurious emission within a 100 kHz bandwidth must be less than  $-70$  dBc relative to the carrier power in the same bandwidth. This is measured using a peak hold setting on the spectrum analyzer, which is equivalent to about  $-80$  dBc when using averaging.

Table 2 shows the equivalent standards for amplifiers, which are in compliance with the 3GPP standards. This table summarizes the key spectral constraints on these units. It can be seen that ACP measured in a 1 MHz bandwidth centered at 4 MHz from the carrier is the most challenging specification.

#### **Agilent Technologies**

Santa Rosa, California 95403 USA

Roland Hassun, Nicholas Kuhn

and

#### **Powerwave Technologies**

Irvine, California 92614 USA

Richard Posner, Richard Sweeney,  
and Bill Vassilakis

To meet these challenging standards especially in the presence of multiple carriers, power amplifier manufacturers such as Powerwave Technologies, are developing increasingly linear amplifiers. Characterizing amplifiers with spurious rejections in excess of 80 dB has become increasingly difficult. Measurements of these levels of spurious are equal to or even better than the current measurement systems capabilities. To meet the challenge, Powerwave Technologies and Agilent collaborated to design a cancellation technique, which has the potential to add about 30 dB of dynamic range to any measurement system, and facilitate the accurate characterization of this new generation of ultra linear power amplifiers.



**Agilent Technologies**

**Intra Base Station System Intermodulation Requirements**

Power level (dBm)	Maximum relative level (dB) at specified carrier offsets (kHz)			
	RBW & VBW: 30kHz, Averaging over 200 sweeps.		RBW & VBW: 100kHz, Averaging over 200 sweeps.	RBW : 300kHz Detector: Max Hold
	600 to 1200	1200 to 1800	1800 to 6000	>6000
>=43	-70	-73	-75	-70
41	-68	-68	-73	-70
39	-66	-66	-71	-70
37	-64	-64	-69	-70
35	-62	-62	-67	-70
<=33	-60	-60	-65	-70

**Table 1. Relative spurious emission mask requirements for transmission of GSM and/or EDGE signals in a MCPA in accordance with European spectral standards (GSM 11.21 version 7.2.0 Release 1998)**

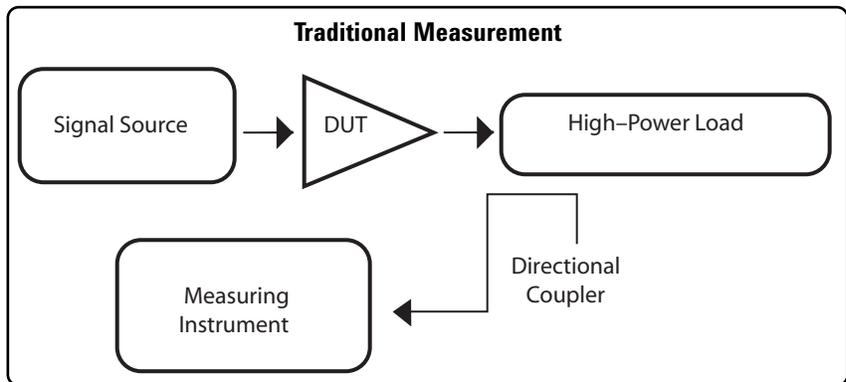
**Spectrum emission mask values, BS maximum output power P ≥ 43 dBm**

Frequency offset of measurement filter – 3 dB point, Δf	Frequency offset of measurement filter center frequency, f_offset	Maximum level	Measurement bandwidth
2.5 ≤ Δf < 2.7 MHz	2.515MHz ≤ f_offset < 2.715 MHz	-14 dBm	30 kHz
2.7 ≤ Δf < 3.5 MHz	2.715MHz ≤ f_offset < 3.515 MHz	-14 -15•(f_offset-2.715) dBm	30 kHz
3.5 ≤ Δf < 7.5 MHz	3.515MHz ≤ f_offset < 4.0 MHz	-26 dBm	30 kHz
7.5 ≤ Δf MHz	4.0MHz ≤ f_offset < 8.0 MHz	-13 dBm	1 kHz
	8.0MHz ≤ f_offset < f_offset_max MHz	-13 dBm	1 kHz

**Table 2. Spectral Mask requirements for 3GPP amplifiers**

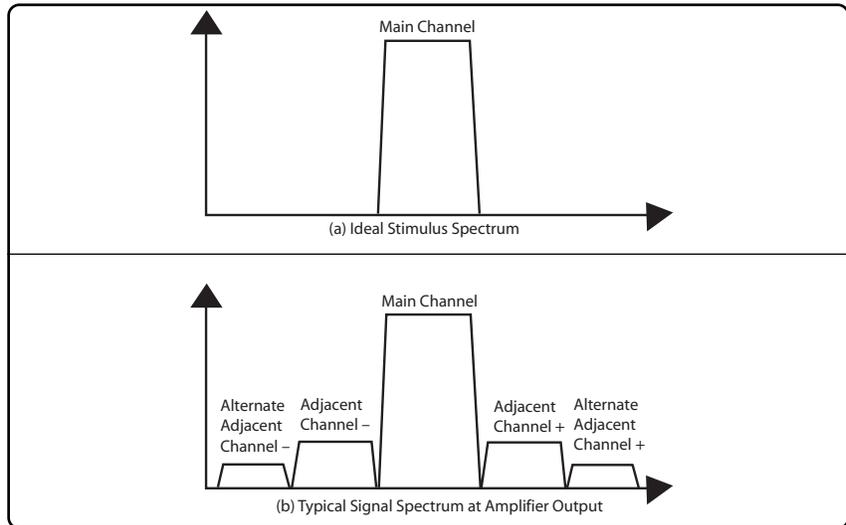
**II. Limitations of existing test methods**

Figure 1 shows a typical setup for measuring ACP (adjacent channel power) and inter-modulation distortion (IMD) of a base-station power amplifier. The output of the DUT is connected to a high-power load and a portion of the output signal is coupled to the measuring instrument. The coupled level to the measuring instrument, typically a spectrum analyzer, is proportional with its input power level. A precision calibrated coupler is used so that the absolute power at the output of the amplifier may be precisely measured.



**Figure 1. High-power amplifier measurement setup**

## II. Limitations of existing test methods (continued)



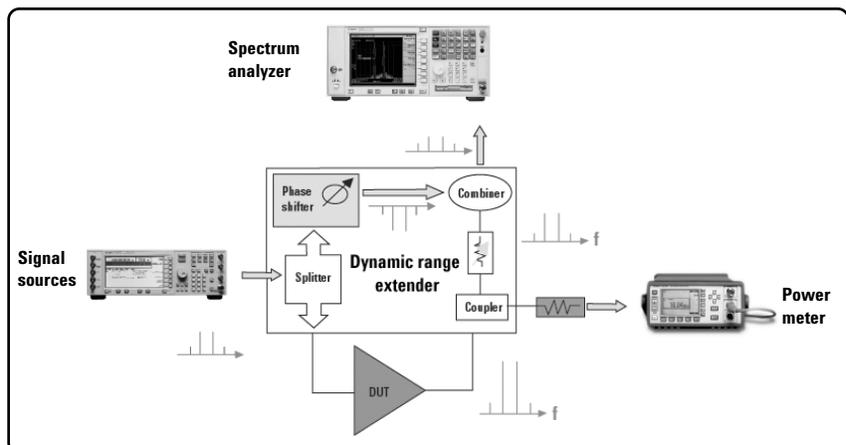
**Figure 2a and 2b. Signal spectrum patterns**

Under ideal measurement conditions, the input to the DUT would have a spectrum that would contain spectral components only in the desired signal channel, as shown in figure 2(a). The DUT, however, has non-linearities that cause the desired spectral components of the signal to mix with each other and with other signals to create additional spectral components. These extra components result in spurious spectral energy in the adjacent channels as indicated in figure 2(b). This is the spectral power that must be measured. Another common term for such power is "spectral regrowth". A measurement system must be able to determine the ratio of the spurious spectrum to that of the desired spectrum and/or the absolute power of the spurious spectrum. The problem is that the power difference between the main channel and the adjacent channel of ultra-linear MCPAs exceeds the dynamic range capability of typical broadband measurement systems. Once the dynamic range of the measurement system is exceeded, the internal IMD generated in the signal source and the measuring instrument, which are similar to that generated in the DUT, results in additional spurious that mask the effects in the DUT. This limits accurate measurement of the DUT performance.

## III. Discussion of dynamic range extender (DRE)

### A. Theory of operation

This measurement technique uses a cancellation signal during part of the process to remove unwanted signal components from the measurement. Figure 3 shows the measurement setup where the source signal is split into two paths; one path is to a phase shifter to provide cancellation and the other un-altered path to the DUT. Maximum cancellation occurs when the two paths have equal magnitude and time delay with opposite phase. Agilent's PSA-series spectrum analyzer is optimized with the test set to provide a real-time display readout of ACPR/ACLR.



**Figure 3. Proposed measurement system**

### III. Discussion of dynamic range extender (DRE) (continued)

In step one, a reference signal is obtained from the DUT by disabling the cancellation signal through the lower path. This establishes the reference power for the ratio measurement. In step two, the leveled and conditioned loop signal is applied to the coupled DUT signal, producing a signal cancellation to the spectrum analyzer. Cancellation occurs when the signal conditions along the two paths are equal both in magnitude and time delay, but opposite in phase. The cancellation subtracts at least 25 dB of the linearly amplified input spectrum to the measuring instrument. This improves the analyzer's dynamic range by allowing its internal attenuation to be reduced, without consequence of self generated non-linearities. The cancellation also subtracts spurious spectral power generated by the signal sources. The cancellation, however, has no effect on the distortion products caused by the DUT. The DUT spectral components are generated inside the loop and cannot be subtracted, so they are still present at the measuring instrument. Cancellation should now be viewed as "the removal of 25 dB of the linearly amplified input stimulus spectrum" to the spectrum analyzer. This allows measurement of both the lower noise floor and the DUT spectral contribution (independent of the input contribution).

In general, use of the measurement system offers the following benefits:

- Spurious and noise contributions from the spectrum analyzer and the input signal are greatly reduced.
- Only spurious products generated by the DUT are measured.

#### B. Bandwidth of cancellation

Optimal operating band cancellation occurs when the two signals that are summed in the power combiner of figure 3 are precisely equal, both in amplitude and time delay, but opposite in phase (180° apart). The approach to achieving phase reversal in the Agilent 8760A KE4 results in a 30 dB cancellation bandwidth in excess of 100 MHz.

### IV. Measurement results with DRE

This ultra-linear wideband amplifier (figure 4.) has been designed to handle the multiple GSM channels required for new multi-carrier base station operation.



Figure 4. Illustrates a 30-watt DCS1800 GSM MCPA

#### IV. Measurement results with DRE (continued)

Figure 5 shows the RF output spectrum of the GSM MCPA with four independent +39.3 dBm GSM-modulated signals at 5 MHz separation for a total RF output power level of 45.3 dBm (33.9 Watts). The right tone value on the signal analyzer is at -1.7 dBm and represents the reference for the measurement.

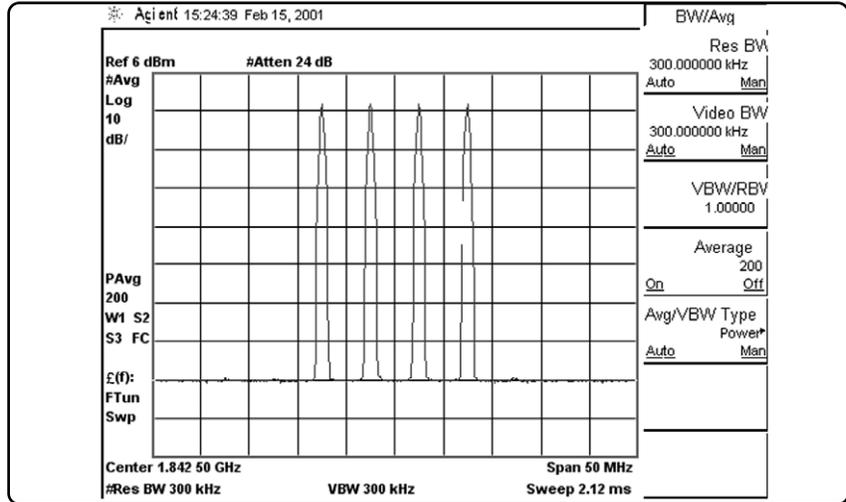


Figure 5. GSM output spectrum

Figure 6 shows that the carrier cancellation due to the DRE is greater than 30 dB and reveals a number of intermodulation components that were not visible in Figure 5. Note also that the ratio of carrier to intermodulation is  $\geq 80$  dB, for the test data above 6 MHz (the specification is -70 dB with (max hold)).

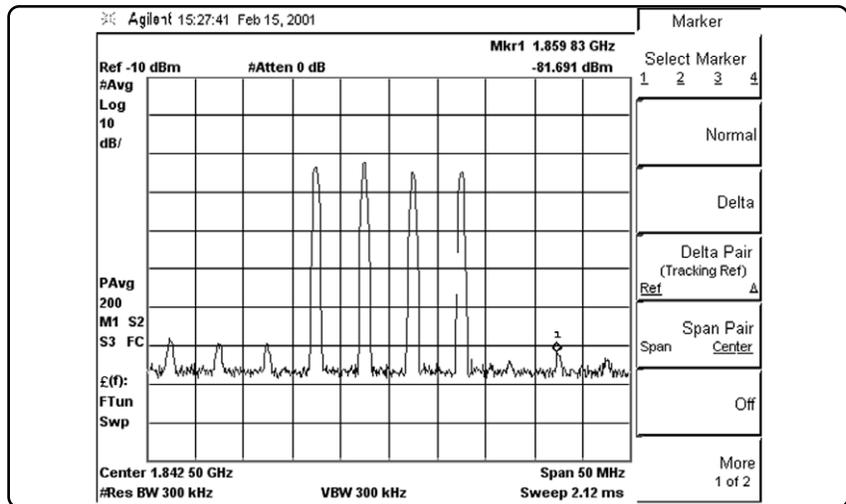


Figure 6. GSM spectrum after cancellation

The additional dynamic range provided with the DRE shows that the spurious signal is 80 dB below the GSM output spectrum as measured using peak hold on the spectrum analyzer. Without use of the DRE, the MCPA output level would exceed the dynamic range of the spectrum analyzer and not allow the spurious products to be seen or measured.

Similar types of comparisons can be made for amplifiers utilizing 3GPP waveforms. Figures 7 to 9 show measurements made on a 3G amplifier operating in the 2.11 to 2.17 GHz frequency range. These measurements were made for the power level in adjacent channels ( $\pm 4$  MHz from center frequency over a 1 MHz bandwidth). These measurements were made for three W-CDMA carriers combined for a total RF output power level of 46.5 dBm (45 Watts).

#### IV. Measurement results with DRE (continued)

Figure 7 shows the direct measurement of the RF output spectrum without the DRE. As shown, the ACP levels at  $\pm 4$  MHz are shown to be approximately  $-16$  dBm. This level is very close to the specified  $-13$  dBm limit. Figure 8 shows  $-24$  dBm after cancellation.

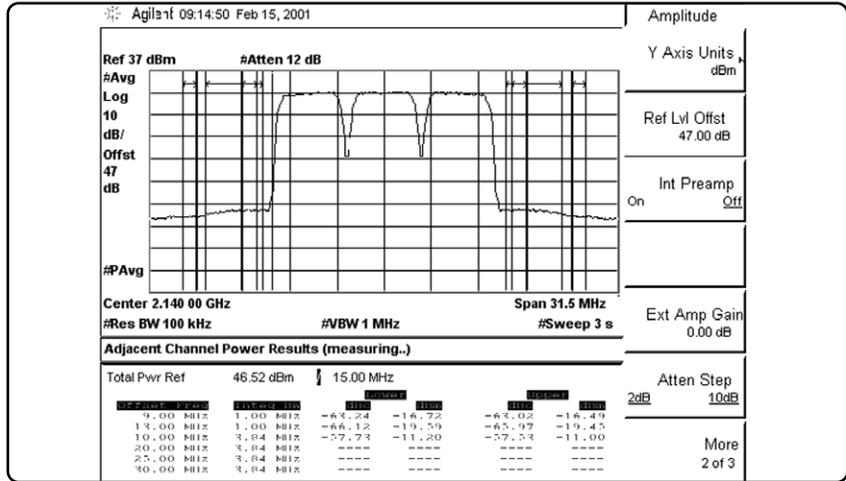


Figure 7. W-CDMA with 3 carriers prior to cancellation

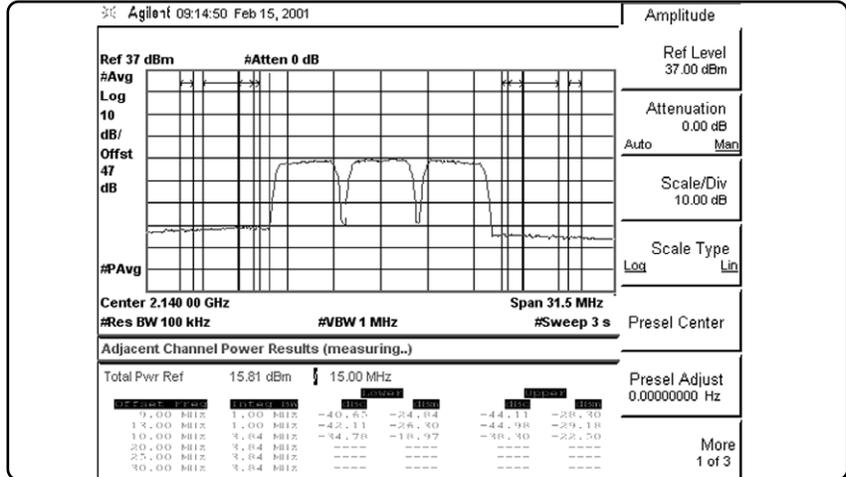


Figure 8. Same as Figure 7, but after cancellation

Figure 9 shows the cancelled measurement when the total RF Output power has been reduced by 1 dB. The ACP levels are now less than  $-35$  dBm indicating that without the DRE, the error would have been greater than 18 dB and allowing the augmented measurement system to demonstrate the effects of Power Amplifier compression on the output spectrum.

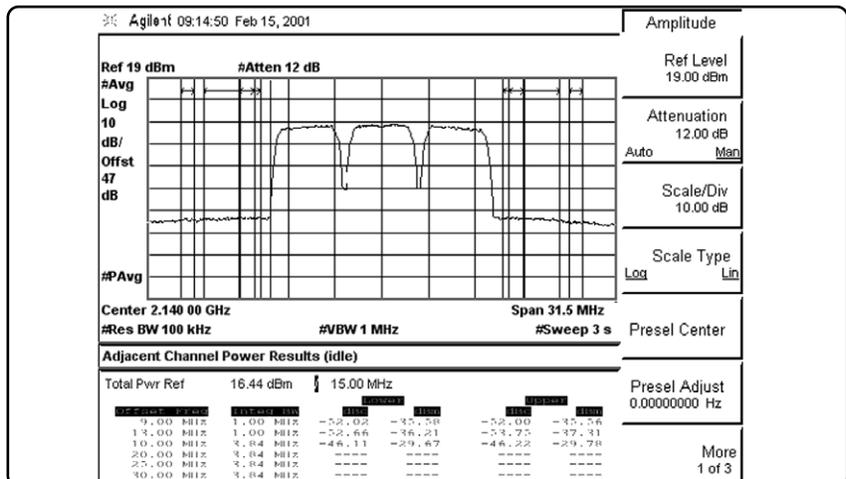


Figure 9. Output power reduced 1 dB, ACP reduced at least 7 dB

## V. Conclusion

The challenge of achieving compliance with very stringent wireless transmission standards has resulted in the development of both extremely linear multi-carrier power amplifiers and of a new measurement instrument to facilitate proper characterization of these new MCPA designs. It has been shown that the new cancellation technique increases the range of intermodulation distortion measurement, including ACPR, by at least 25 dB over traditional IMD measurements. The cancelled signal removes most of the stimulus source IMD effect from the distortion-measuring instrument. The cancelled signal also reduces the power level to the spectrum analyzer by the same amount so that it can operate with less attenuation at its input. Less attenuation reduces the measuring instrument's effective noise figure and increases its dynamic range.

The examples in this paper show improvement in excess of 11 dB in the measurement of spurious spectral products, ACPR, and noise power ratio measurements.

**By internet, phone, or fax, get assistance  
with all your test and measurement needs.**

**Online assistance:**

**[www.agilent.com/find/assist](http://www.agilent.com/find/assist)**

**Phone or Fax**

**United States:**

(tel) 1 800 452 4844

**Canada:**

(tel) 1 877 894 4414

(fax) (905) 282-6495

**Europe:**

(tel) (31 20) 547 2323

(fax) (31 20) 547 2390

**Japan:**

(tel) (81) 426 56 7832

(fax) (81) 426 56 7840

**Latin America:**

(tel) (305) 269 7500

(fax) (305) 269 7599

**Australia:**

(tel) 1 800 629 485

(fax) (61 3) 9210 5947

**New Zealand:**

(tel) 0 800 738 378

(fax) 64 4 495 8950

**Asia Pacific:**

(tel) (852) 3197 7777

(fax) (852) 2506 9284

**Product specifications and descriptions  
in this document subject to change  
without notice.**

**Copyright © 2001**

**Agilent Technologies**

**Printed in USA June 26, 2001**

**5988-2978EN**



**Agilent Technologies**