Introduction

In hard disk drives, digital information is stored and retrieved magnetically by a “read head” which flies over the disk within tens of nanometers of its surface. Figure 1 is a photograph of a read head and hard disk together. To protect the magnetic material in which information is stored, a hard overcoat is applied to the surface which may be as thin as just a few nanometers. The hard overcoat protects the underlying material by acting both as a lubricant and a mechanical barrier. Hard-disk manufacturers are keenly interested in measuring the mechanical properties of such overcoats in order to gain knowledge for product improvement, and instrumented indentation has emerged as the technique of choice for making these measurements. However, indentation results for the overcoat are inevitably lower than the true values, because the coating is so thin. That is, some of the deformation from the indentation test is accommodated by the material under the coating of interest, which makes the coating appear more compliant than it actually is.

Without any correction for influence of the underlying material, one faces a compromise between uncertainty and error. At very small displacements, the error due to the substrate influence may be small, but the uncertainty is greater due to surface roughness, tip variations, vibration, temperature variations, etc. As indentation depth increases, the uncertainty decreases, but the error due to substrate influence increases. Thus, the purpose of this work was to apply an analytic model to the analysis of hard coatings tested by instrumented indentation in order to obtain the Young’s modulus of the film alone. In a previous application note, such a model was introduced and verified by finite-element analysis. Hereafter, this model will be called the “Hay-Crawford” model.

The Hay-Crawford model provides an analytic means for accounting for substrate influence on measured modulus. The details of this model are explained in another application note; here, we shall summarize by telling the inputs and output of the model. The inputs to the model are:

- The apparent (substrate-affected) Young’s modulus as measured by the method of Oliver and Pharr,
- Film thickness,
- Poisson’s ratio of the film,
- Young’s modulus of the substrate, and
- Poisson’s ratio of the substrate.

The output of the model is the substrate-independent Young’s modulus of the film. (Note: Although the Poisson’s ratios of film and substrate are required inputs, the output of the model is rather insensitive to these parameters.)

In this work, we tested and analyzed two samples provided by Seagate Technology, a major manufacturer of hard disk drives. The samples were produced for the purpose of evaluating the Hay-Crawford model for substrate influence. As such, the coatings tested in this work were substantially thicker than overcoats for an actual hard disk. Also, the coatings were deposited on silicon rather than magnetic media. These simplifications allowed for a rigorous evaluation of the model, because substrate influence was slight at shallow depths, and because the substrate properties were well known.
Experimental Method

Samples

Two silicon-carbide (SiC) films on silicon were tested; the thickness of the first film was 150nm and the thickness of the second film was 300nm. The SiC films were deposited onto prime silicon substrates using an industrial PVD system equipped with a planar magnetron sputter source and 99.99% pure silicon carbide target. For these samples, a value of 170GPa was used for the substrate Young’s modulus.

Equipment and Procedure

The SiC films were tested in a Keysight Technologies, Inc. lab with a Keysight G200 NanoIndenter, utilizing the CSM option and a DCM head fitted with a Berkovich indenter. Results were achieved using the NanoSuite test method “G-Series DCM CSM for Thin Films”. This test method implements the Hay-Crawford model to achieve substrate-independent measurements of Young’s modulus. It should be noted that this method does not correct measurements of hardness for substrate influence. However, hardness measurements are generally less sensitive to substrate influence, because the extent of the plastic field is much smaller than the extent of the elastic field. Even when there is a substantial difference between film hardness and substrate hardness, the hardness measured at 20% of the film thickness usually manifests negligible substrate influence.

Keysight Nanolndenters have been the industry choice for thin-film testing precisely because of the continuous stiffness measurement (CSM) option, which measures elastic contact stiffness ($A$) dynamically. With the CSM option, every indentation test returns complete depth profiles of Young’s modulus and hardness. Using this option, ten tests were performed on each sample. Loading was controlled such that the loading rate divided by the load ($P'/P$) remained constant at 0.05/sec; loading was terminated at a penetration depth of 200nm or greater. The excitation frequency was 75Hz, and the excitation amplitude was controlled such that the displacement amplitude remained constant at 1nm.

<table>
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<th>Thickness (nm)</th>
<th>$E_f$ (GPa)</th>
<th>$\sigma(E_f)$ (GPa)</th>
<th>$E_a$ (GPa)</th>
<th>$\sigma(E_a)$ (GPa)</th>
<th>$\sigma(E_f-E_a)/E_a$ %</th>
<th>$E_f/E_a$</th>
<th>$H$ (GPa)</th>
<th>$\sigma(H)$ (GPa)</th>
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<td>230</td>
<td>6.5</td>
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<td>1.67</td>
<td>19.1</td>
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</table>

Table 1. Summary of experimental results for SiC coatings on silicon. The true Young’s modulus of the film ($E_f$) is about 25% higher than the apparent Young’s modulus ($E_a$) when the indentation depth is 20% of the film thickness.

Figure 2. Analytical sequence for the two samples of SiC on Si showing (a) Apparent (substrate-affected) modulus as a function of indenter penetration, (b) Apparent modulus and film modulus as a function of normalized indenter penetration, and (c) Values at 20% of film thickness. Note: In (a) and (b), the trace for each sample represents the average of all tests on that sample. For clarity, error bars spanning one standard deviation are shown only on the bar chart (c).
Result and Discussion

Results are summarized in Table 1. Figure 2 shows the progression of elastic analysis for the two samples. Figure 2a shows the apparent Young’s modulus achieved by standard analysis as a function of indentation depth. As expected, the Young’s modulus for the thinner sample decays faster as a function of depth. Figure 2b shows both the apparent Young’s modulus (solid symbols) and the Young’s modulus of the film alone (open symbols) plotted as a function of normalized indentation depth. The fact that the two samples look exactly the same when plotted this way tells us that substrate influence has not been accounted, but such accounting seems unnecessary, because hardness reaches its plateau at about 20% of the film thickness. In these results, substrate influence has not been accounted, but such accounting seems unnecessary, because hardness reaches its plateau at about 20% of the film thickness. Note: In (a) and (b), the trace for each sample represents the average of all tests on that sample. For clarity, error bars spanning one standard deviation are shown only on the bar chart (c).

Figure 3 shows results for hardness. These results have not been adjusted for substrate influence, but as expected, no adjustment is necessary. The hardness reaches its plateau at about 20% of the film thickness. For hard materials, it is important to remember that hardness is defined as the mean pressure of the contact, or load divided by contact area under load: \( H = \frac{P}{A} \). When the contact is substantial elastic, the Hertzian contact model tells us that the mean pressure (pm) goes as the square root of displacement. Therefore, we should not be surprised that the measured hardness (which we have defined as pm) goes to zero as the displacement goes to zero. This simply means that at these small displacements, the contact is substantially elastic, and so the reported “hardness” has little to do with the plastic properties of the film.
Conclusions

The Keysight G200 NanoIndenter with a DCM head is the industry choice for these measurements because of its high-precision, speed, ease of use, and the CSM option, which delivers properties as a continuous function of penetration depth. In this work, NanoSuite Explorer was used to implement an analytic model which accounts for substrate influence on the measurement of Young's modulus. Test methods with this analysis are now available to customers with NanoSuite Professional.

Having a model which accounts for substrate influence on Young's modulus affords several practical advantages:

- Reported moduli are for the film alone,
- Less user influence, because depth range for calculating moduli does not have to be selected “by eye”, and
- Less uncertainty, because results are obtained at deeper penetration depths.

Measurements of hardness were not adjusted for substrate influence, but no such adjustment was necessary; for these samples, hardness reaches its plateau at about 20% of the film thickness. This is as expected, because the extent of the plastic field is smaller than the extent of the elastic field. Thus, when testing similar materials with a test method that implements the Hay-Crawford model, both the Young’s modulus and hardness should be obtained at an indentation depth that is 20% of the film thickness.

References


Nano Mechanical Systems from Keysight Technologies

Keysight Technologies, the premier measurement company, offers high-precision, modular nano-measurement solutions for research, industry, and education. Exceptional worldwide support is provided by experienced application scientists and technical service personnel. Keysight’s leading-edge R&D laboratories ensure the continued, timely introduction and optimization of innovative, easy-to-use nanomechanical system technologies.